## EQUATIONS OF THE LINEAR THEORY OF ELASTICITY OF ANISOTROPIC MATERIALS, REDUCED TO THREE INDEPENDENT WAVE EQUATIONS

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Characteristic operators and vectors for the system of differential equations of the linear theory of elasticity were introduced in [1-3]. Determination of the operators and vectors was reduced in [3] to a special coupled eigenvalue problem for six numerical matrices comprising the components of the elastic modulus tensor. Here, we propose a method of structuring the matrix of the operators of the linear theory of elasticity for anisotropic materials in such a way as to permit reduction of the initial system to three independent wave equations. We find specific classes of anisotropic materials that depend on arbitrary parameters. In particular, we obtain formulas to describe an elastic anisotropic medium (generalization of a Green medium) with longitudinal and transverse waves for any direction of the wave normal. Formulas for special orthotropic and transversely isotropic materials are also obtained.

With arbitrary anisotropy and an absence of body forces, the equations of the theory of elasticity appear as follows in orthotropic cartesian coordinates  $x_1$ ,  $x_2$ ,  $x_3$  [4]

$$L_{ij}\mu_{j} = 0, \ L_{ij} = L_{ji} = A_{i(k)j}\partial_{kl} - \rho\delta_{ij}\partial_{...},$$
(1)

where  $u_j$  is the displacement vector;  $A_{i(kl)j} = (A_{iklj} + A_{ilkj})/2$ ;  $A_{iklj} = A_{kilj} = A_{ljik}$  is the constant tensor of the elastic moduli;  $\rho$  is the constant density of the material;  $\delta_{ij}$  is the Kronecker symbol;  $\partial$  and  $\partial_k$  are derivatives with respect to time and the coordinate  $x_k$ ; repeating letter subscripts denote summation. The properties of the coefficients  $A_{i(kl)j}$  were studied in [5-7].

For operators (1), we attempt to find differential matrices  $T = [t_{jp}]$ ,  $D = diag(D_1, D_2, D_3)$  with constant coefficients such that LT = TD,  $|T| \neq 0$ . Then the general solution of Eqs. (1) will be as follows:  $u = T\varphi$ ,  $D\varphi = f$ , Tf = 0. The formulas  $u = T\varphi$ ,  $\varphi = T'\tilde{u}$  (the prime denoting transposition) transpose the solutions of the equations Lu = 0,  $D\varphi = 0$  [2, 3]. The expression  $u = TT'\tilde{u}$  is the formula for obtaining new solutions, i.e. Q = TT' is a symmetry operator in the sense of group analysis [8].

Let  $D_1 = a_{kl}^{(1)} \partial_{kl} - \rho \partial_{...} a_{kl}^{(1)} = a_{lk}^{(1)}, t_{jl} = \alpha_{js} \partial_s$  We then write the relation LT = TD in the form

$$(A_{i(k)j} - \delta_{ij} a_{kl}^{(1)}) \alpha_{ji} \partial_{klr} = 0.$$
<sup>(2)</sup>

Reducing similar terms in (2) and equating the coefficients with  $\partial_{kls}$  to zero, we can use (2) to obtain [3, 9] a special coupled eigenvalue problem for six matrices  $A^{(1)} = A_{i(11)j}, \dots, A^{(6)} = \sqrt{2A_{i(12)j}}$ :

$$\begin{aligned} &(A_{i(11)j} - \delta_{ij}a_{11})\alpha_{j1} = 0, \ (A_{i(22)j} - \delta_{ij}a_{22})\alpha_{j2} = 0, \\ &(A_{i(33)j} - \delta_{ij}a_{33})\alpha_{j3} = 0; \\ &2(A_{i(23)j} - \delta_{ij}a_{23})\alpha_{j2} + (A_{i(22)j} - \delta_{ij}a_{22})\alpha_{j3} = 0, \\ &(A_{i(33)j} - \delta_{ij}a_{33})\alpha_{j2} + 2(A_{i(23)j} - \delta_{ij}a_{23})\alpha_{j3} = 0; \\ &2(A_{i(13)j} - \delta_{ij}a_{13})\alpha_{j1} + (A_{i(11)j} - \delta_{ij}a_{11})\alpha_{j3} = 0, \\ &(A_{i(33)j} - \delta_{ij}a_{33})\alpha_{j1} + 2(A_{i(13)j} - \delta_{ij}a_{13})\alpha_{j3} = 0; \end{aligned}$$

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$$2(A_{i(12)j} - \delta_{ij}a_{12})\alpha_{j1} + (A_{i(11)j} - \delta_{ij}a_{11})\alpha_{j2} = 0,$$
  

$$(A_{i(22)j} - \delta_{ij}a_{22})\alpha_{j1} + 2(A_{i(12)j} - \delta_{ij}a_{12})\alpha_{j2} = 0;$$
  

$$2[(A_{i(23)j} - \delta_{ij}a_{23})\alpha_{j1} + (A_{i(13)j} - \delta_{ij}a_{13})\alpha_{j2} + (A_{i(12)j} - \delta_{ij}a_{12})\alpha_{j3}] = 0.$$
(3)

Here,  $a_{kl} = a_{kl}^{(1)}$ . System (3) consists of 30 equations and is difficult to solve directly. However, if we assign  $\alpha_{js}$ , then it becomes fairly simple to find the eigenvalues  $a_{kl}$  and the corresponding matrices  $A^{(1)}$ , ...,  $A^{(6)}$  and, thus [6, 7], the matrices  $A_{ji}$  of the elastic moduli in the generalized Hooke's law.

The matrix T has the following structure [3]:

$$T = [\alpha_{js}\partial_{s}, \beta_{jp}\partial_{p}, \epsilon_{jmn}\alpha_{m}\beta_{np}\partial_{sp}]$$
(4)

 $(\varepsilon_{imn} \text{ are Levi-Civita symbols}), while$ 

$$\alpha'\beta + \beta'\alpha = 0 \tag{5}$$

is the condition of orthogonality of the columns  $t_{j1}$ ,  $t_{j2}$ . It follows from (5) that  $\alpha'\beta = c$  is an antisymmetric matrix (c' = -c). If  $|\alpha| \neq 0$ , then  $\beta = (\alpha')^{-1}c = (\alpha')^{-1}\alpha'\tilde{c}\alpha = \tilde{c}\alpha$ ,  $\tilde{c}' = -\tilde{c}$ . Matrix (4) can be written as

$$T = [t_{j1}, e_{jmn}c_m t_{n1}, c_j t_{p1} t_{p1} - c_n t_{n1} t_{j1}],$$
(6)

where  $t_{j1}$  and  $c_m$  are arbitrary non-colinear vectors. The determinant of matrices (4) and (6) has the form

$$|T| = t_{j3}t_{j3} = (t_{i1}t_{i1})(t_{k2}t_{k2}) = (t_{i1}t_{i1})(c_m c_m t_{n1}t_{n1} - c_m t_{m1}c_{n1}t_{n1})$$

Let a certain symmetric matrix A be represented in terms of eigenvalues and orthonormalized eigenvectors ( $f_{ip}f_{iq} = \delta_{pq}$ ):

$$A = F\Lambda F' \rightarrow \Lambda = F'AF, \lambda_{pq} = A_{ij}f_{ip}f_{jq}$$

We use this to obtain the following eigenvalues for p = q

λ<sup>(1)</sup>

$$\lambda_{11} = A_{ij}f_{i1}f_{j1}, \lambda_{22} = A_{ij}f_{i2}f_{j2}, \lambda_{33} = A_{ij}f_{i3}f_{j3},$$
(7)

For  $p \neq q$ 

$$\lambda_{21} = A_{ij}f_{i2}f_{j1} = 0, \ \lambda_{31} = A_{ij}f_{i3}f_{j1} = 0, \lambda_{32} = A_{ij}f_{i3}f_{j2} = 0.$$
(8)

Conditions (8) are necessary and sufficient for  $f_{ip}$  to be eigenvectors, while expressions (7) give the eigenvalues of matrix A. As was shown in [3], the matrices  $A^{(1)}$ ,  $A^{(2)}$ , and  $A^{(3)}$  correspond to the characteristic (non-normalized) vectors

$$[\alpha_{j1}, \beta_{j1}, \varepsilon_{jmn} \alpha_{m1} \beta_{n1}],$$

$$[\alpha_{j2}, \beta_{j2}, \varepsilon_{jmn} \alpha_{m2} \beta_{n2}], [\alpha_{j3}, \beta_{j3}, \varepsilon_{jmn} \alpha_{m3} \beta_{n3}].$$

$$(9)$$

Taking Eqs. (3) and (7)-(9) into account, we find the eigenvalues of  $A^{(1)}$ ,  $A^{(2)}$ , and  $A^{(3)}$  and the conditions under which expressions (9) are eigenvectors of these matrices. We thus obtain

$$a_{11}^{(1)} = \frac{A_{i(11)j}\alpha_{i1}\alpha_{j1}}{\alpha_{s1}\alpha_{s1}}, \ a_{11}^{(2)} = \frac{A_{i(11)j}\beta_{i1}\beta_{j1}}{\beta_{s1}\beta_{s1}},$$

$$a_{11}^{(3)} = \frac{A_{i(11)j}\varepsilon_{imn}\alpha_{m1}\beta_{n1}\varepsilon_{jpq}\alpha_{p1}\beta_{q1}}{\alpha_{s1}\alpha_{s1}\beta_{s1}\beta_{s1}};$$

$$= A_{i(11)j}\alpha_{i1}\beta_{j1} = 0, \ \lambda_{31}^{(1)} = A_{i(11)j}\alpha_{i1}\varepsilon_{jmn}\alpha_{m1}\beta_{n1} = 0,$$

$$\lambda_{32}^{(1)} = A_{i(11)j}\beta_{i1}\varepsilon_{jmn}\alpha_{m1}\beta_{n1} = 0$$
(11)

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(here and below, we omit the normalizing factors);

$$a_{22}^{(1)} = \frac{A_{i(22)j}\alpha_{i2}\alpha_{j2}}{\alpha_{s2}\alpha_{s2}}, \ a_{22}^{(2)} = \frac{A_{i(22)j}\beta_{i2}\beta_{j2}}{\beta_{s2}\beta_{s2}}, \tag{12}$$

$$a_{22}^{(3)} = \frac{A_{i(22)j}\varepsilon_{inn}\alpha_{m2}\beta_{n2}\varepsilon_{jp}\alpha_{p2}\beta_{q2}}{\alpha_{s2}\alpha_{s2}\beta_{s2}\beta_{r2}\beta_{r2}};$$

$$A = \alpha_{s}\beta_{s} = \Omega_{s}\lambda^{(2)} = A = \alpha_{s}\varepsilon_{s}\alpha_{s}\beta_{s} = 0$$
(13)

$$\lambda_{21}^{(2)} = A_{i(22)j} \alpha_{i2} \beta_{j2} = 0, \ \lambda_{31}^{(2)} = A_{i(22)j} \alpha_{i2} \epsilon_{jmn} \alpha_{m2} \beta_{n2} = 0,$$

$$\lambda_{32}^{(2)} = A_{i(22)j} \beta_{i2} \epsilon_{jmn} \alpha_{m2} \beta_{n2} = 0;$$
(13)

$$a_{33}^{(1)} = \frac{A_{i(33)j}\alpha_{i3}\alpha_{j3}}{\alpha_{i3}\alpha_{i3}}, a_{33}^{(2)} = \frac{A_{i(33)j}\beta_{i3}\beta_{j3}}{\beta_{i3}\beta_{i3}},$$
(14)

$$a_{33}^{(3)} = \frac{A_{i(33)j}}{\alpha_{33}} a_{j3} \frac{\beta_{j3}}{\beta_{j3}} - \beta_{j3} \frac{\beta_{j3}}{\beta_{j3}} \frac{\beta_{j3}}{\beta_{j3}} \frac{\beta_{j3}}{\beta_{j3}};$$
  

$$\lambda_{21}^{(3)} = A_{i(33)j} \alpha_{i3} \beta_{j3} = 0, \lambda_{31}^{(3)} = A_{i(33)j} \alpha_{i3} \varepsilon_{jmn} \alpha_{m3} \beta_{n3} = 0,$$
  

$$\lambda_{32}^{(3)} = A_{i(33)j} \beta_{i3} \varepsilon_{jmn} \alpha_{m3} \beta_{n3} = 0.$$
(15)

Expressions (9) will be eigenvectors for  $A^{(1)}$ ,  $A^{(2)}$ , and  $A^{(3)}$  if conditions (11), (13), and (15) are satisfied. The eigenvalues are then given by Eqs. (10), (12), and (14).

Since the matrices  $A_{i(kl)j}$  are symmetric, then if we multiply Eqs. (3) by the corresponding columns of  $\alpha_{is}$ ,  $\beta_{ip}$  and take the first three equations into account, we can use (3) to obtain

$$a_{23}^{(1)} = \frac{A_{i(23)j}\alpha_{i2}\alpha_{j2}}{\alpha_{m2}\alpha_{m2}} = \frac{A_{i(23)j}\alpha_{i3}\alpha_{j3}}{\alpha_{n3}\alpha_{n3}},$$

$$a_{13}^{(1)} = \frac{A_{i(13)j}\alpha_{i1}\alpha_{j1}}{\alpha_{m1}\alpha_{m1}} = \frac{A_{i(12)j}\alpha_{i3}\alpha_{j3}}{\alpha_{n3}\alpha_{n3}},$$

$$a_{12}^{(1)} = \frac{A_{i(12)j}\alpha_{i1}\alpha_{j1}}{\alpha_{m1}\alpha_{m1}} = \frac{A_{i(12)j}\alpha_{i2}\alpha_{j2}}{\alpha_{n2}\alpha_{n2}};$$

$$a_{23}^{(2)} = \frac{A_{i(23)j}\beta_{j2}\beta_{j2}}{\beta_{m2}\beta_{m2}} = \frac{A_{i(23)j}\beta_{i3}\beta_{j3}}{\beta_{n3}\beta_{n3}},$$

$$a_{13}^{(2)} = \frac{A_{i(13)j}\beta_{i1}\beta_{j1}}{\beta_{m1}\beta_{m1}} = \frac{A_{i(12)j}\beta_{i2}\beta_{j2}}{\beta_{n2}\beta_{n2}},$$
(16)
$$a_{12}^{(2)} = \frac{A_{i(12)j}\beta_{i1}\beta_{j1}}{\beta_{m1}\beta_{m1}} = \frac{A_{i(12)j}\beta_{i2}\beta_{j2}}{\beta_{n2}\beta_{n2}}.$$

It is evident from (16) that the following conditions must be satisfied

$$\begin{aligned} A_{i(23)j} &\left( \frac{\alpha_{ij}\alpha_{j2}}{\alpha_{m2}\alpha_{m2}} - \frac{\alpha_{ij}\alpha_{j3}}{\alpha_{n3}\alpha_{n3}} \right) = 0, \\ A_{i(13)j} &\left( \frac{\alpha_{i1}\alpha_{j1}}{\alpha_{m1}\alpha_{m1}} - \frac{\alpha_{ij}\alpha_{j3}}{\alpha_{n3}\alpha_{n3}} \right) = 0, \\ A_{i(12)j} &\left( \frac{\alpha_{i1}\alpha_{j1}}{\alpha_{m1}\alpha_{m1}} - \frac{\alpha_{ij}\alpha_{j2}}{\alpha_{n2}\alpha_{n2}} \right) = 0; \\ A_{i(23)j} &\left( \frac{\beta_{i2}\beta_{j2}}{\beta_{m2}} - \frac{\beta_{i3}\beta_{j3}}{\beta_{n3}\beta_{n3}} \right) = 0, \\ A_{i(13)j} &\left( \frac{\beta_{i1}\beta_{j1}}{\beta_{m1}\beta_{m1}} - \frac{\beta_{i3}\beta_{j3}}{\beta_{n3}\beta_{n3}} \right) = 0, \\ A_{i(12)j} &\left( \frac{\beta_{i1}\beta_{j1}}{\beta_{m1}\beta_{m1}} - \frac{\beta_{i2}\beta_{j2}}{\beta_{n2}\beta_{n2}} \right) = 0; \end{aligned}$$
(17)

In (4), the third column has the form  $t_{j3} = \gamma_{j(sp)} \partial_{sp}$ , where:

$$\gamma_{j(sp)} = \frac{1}{2} \varepsilon_{jmn} (\alpha_{ms} \beta_{np} + \alpha_{mp} \beta_{ns}).$$
(18)

We now write the relation analogous to (2):

$$(A_{i(kl)j} - \delta_{ij}a_{kl}^{(3)})\gamma_{j(sp)}\partial_{klsp} = 0.$$
<sup>(19)</sup>

Reducing similar terms in (19) and equating the coefficients with  $\partial_{klsp}$  to zero, we obtain the following system of equations from (19)

$$\begin{array}{l} (A_{i(11)j} - \delta_{ij}a_{11})\gamma_{j(11)} = 0, \ (A_{i(22)j} - \delta_{ij}a_{22})\gamma_{j(22)} = 0, \\ (A_{i(33)j} - \delta_{ij}a_{33})\gamma_{j(33)} = 0; \\ 2(A_{i(23)j} - \delta_{ij}a_{23})\gamma_{j(22)} + 2(A_{i(22)j} - \delta_{ij}a_{22})\gamma_{j(23)} = 0, \\ 2(A_{i(23)j} - \delta_{ij}a_{23})\gamma_{j(33)} + 2(A_{i(33)j} - \delta_{ij}a_{33})\gamma_{j(23)} = 0; \\ 2(A_{i(13)j} - \delta_{ij}a_{13})\gamma_{j(11)} + 2(A_{i(11)j} - \delta_{ij}a_{11})\gamma_{j(13)} = 0, \\ 2(A_{i(13)j} - \delta_{ij}a_{13})\gamma_{j(33)} + 2(A_{i(23)j} - \delta_{ij}a_{33})\gamma_{j(13)} = 0; \\ 2(A_{i(12)j} - \delta_{ij}a_{12})\gamma_{j(11)} + 2(A_{i(11)j} - \delta_{ij}a_{11})\gamma_{j(12)} = 0, \\ 2(A_{i(12)j} - \delta_{ij}a_{12})\gamma_{j(22)} + 2(A_{i(22)j} - \delta_{ij}a_{22})\gamma_{j(12)} = 0; \\ (A_{i(11)j} - \delta_{ij}a_{11})\gamma_{j(22)} + (A_{i(22)j} - \delta_{ij}a_{22})\gamma_{j(11)} + 4(A_{i(13)j} - \delta_{ij}a_{13})\gamma_{j(13)} = 0, \\ (A_{i(11)j} - \delta_{ij}a_{11})\gamma_{j(33)} + (A_{i(33)j} - \delta_{ij}a_{33})\gamma_{j(21)} + 4(A_{i(23)j} - \delta_{ij}a_{23})\gamma_{j(13)} = 0, \\ (A_{i(22)j} - \delta_{ij}a_{22})\gamma_{j(33)} + (A_{i(33)j} - \delta_{ij}a_{33})\gamma_{j(22)} + 4(A_{i(23)j} - \delta_{ij}a_{23})\gamma_{j(13)} = 0, \\ (A_{i(22)j} - \delta_{ij}a_{22})\gamma_{j(33)} + (A_{i(33)j} - \delta_{ij}a_{33})\gamma_{j(22)} + 4(A_{i(23)j} - \delta_{ij}a_{23})\gamma_{j(13)} = 0, \\ (A_{i(22)j} - \delta_{ij}a_{22})\gamma_{j(33)} + (A_{i(33)j} - \delta_{ij}a_{33})\gamma_{j(22)} + 4(A_{i(23)j} - \delta_{ij}a_{23})\gamma_{j(13)} = 0, \\ 2(A_{i(22)j} - \delta_{ij}a_{22})\gamma_{j(13)} + 2(A_{i(23)j} - \delta_{ij}a_{23})\gamma_{j(13)} = 0, \\ 2(A_{i(22)j} - \delta_{ij}a_{23})\gamma_{j(12)} + 4(A_{i(21)j} - \delta_{ij}a_{13})\gamma_{j(22)} + \\ + 4(A_{i(23)j} - \delta_{ij}a_{23})\gamma_{j(12)} + 2(A_{i(13)j} - \delta_{ij}a_{13})\gamma_{j(23)} = 0, \\ 2(A_{i(23)j} - \delta_{ij}a_{33})\gamma_{j(12)} + 2(A_{i(13)j} - \delta_{ij}a_{13})\gamma_{j(23)} = 0, \\ 2(A_{i(23)j} - \delta_{ij}a_{33})\gamma_{j(12)} + 2(A_{i(12)j} - \delta_{ij}a_{13})\gamma_{j(23)} = 0, \\ 2(A_{i(23)j} - \delta_{ij}a_{33})\gamma_{j(12)} + 2(A_{i(12)j} - \delta_{ij}a_{13})\gamma_{j(23)} = 0, \\ 2(A_{i(23)j} - \delta_{ij}a_{33})\gamma_{j(12)} + 2(A_{i(12)j} - \delta_{ij}a_{31})\gamma_{j(23)} = 0. \\ \end{array}$$

Here,  $a_{kl} = a_{kl}^{(3)} = a_{lk}^{(3)}$ . Taking (18) into account, we find that the first three equations of (20) lead to Eqs. (10), (12), (14) for  $a_{11}^{(3)}$ ,  $a_{22}^{(3)}$ ,  $a_{33}^{(3)}$  and conditions (11), (13), (15). Analogously to (16), we find from the other equations of (20) that

$$a_{23}^{(3)} = \frac{A_{i(23)j}'_{i(22)}\gamma_{m(22)}}{\gamma_{m(22)}\gamma_{m(22)}} = \frac{A_{i(23)j}'_{i(33)}\gamma_{i(33)}}{\gamma_{n(33)}\gamma_{n(33)}},$$

$$a_{13}^{(3)} = \frac{A_{i(13)j}'_{i(11)}\gamma_{j(11)}}{\gamma_{m(11)}\gamma_{m(11)}} = \frac{A_{i(13)j}'_{i(33)}\gamma_{i(33)}}{\gamma_{n(33)}\gamma_{n(33)}},$$

$$a_{12}^{(3)} = \frac{A_{i(12)j}'_{i(11)}\gamma_{j(11)}}{\gamma_{m(11)}\gamma_{m(11)}} = \frac{A_{i(12)j}'_{i(22)}\gamma_{j(22)}}{\gamma_{n(22)}\gamma_{n(22)}}.$$
(21)

It is apparent from (21) that the following conditions must be satisfied

$$\begin{aligned} A_{i(23)j} &\left( \frac{\gamma_{i(22)}\gamma_{j(22)}}{\gamma_{m(22)}\gamma_{m(22)}} - \frac{\gamma_{i(33)}\gamma_{j(33)}}{\gamma_{n(33)}\gamma_{n(33)}} \right) = 0, \\ A_{i(13)j} &\left( \frac{\gamma_{i(11)}\gamma_{j(11)}}{\gamma_{m(11)}\gamma_{m(11)}} - \frac{\gamma_{i(33)}\gamma_{j(33)}}{\gamma_{n(33)}\gamma_{n(33)}} \right) = 0, \\ A_{i(12)j} &\left( \frac{\gamma_{i(11)}\gamma_{j(11)}}{\gamma_{m(11)}\gamma_{m(11)}} - \frac{\gamma_{i(22)}\gamma_{j(22)}}{\gamma_{n(22)}\gamma_{n(22)}} \right) = 0. \end{aligned}$$

$$(22)$$

Thus, the algorithm for constructing operators T and D will be as follows. We specify the matrices  $\alpha_{js}$ ,  $\beta_{jp}$ , which are connected by condition (5). We then require satisfaction of necessary conditions (11), (13), (15), (17), (22), which we use to find possible values of the matrices  $A_{i(kl)j}$ . We then use Eqs. (10), (12), (14), (16), and (21) to obtain the coefficients

 $a_{kl}^{(1)}$ ,  $a_{kl}^{(2)}$ ,  $a_{kl}^{(3)}$ . Finally, we check to make sure that all remaining equations of (3) and (20) are satisfied. We used this method and obtained basically new solutions.

The operators T and D were found earlier [2, 3] for isotropic and transversely isotropic materials. Now we construct a general definition of certain classes of anisotropic materials with arbitrary parameters using the operators T and D. To illustrate, if  $\alpha_{js} = \partial_{js}$ , then by following the algorithm and performing all necessary calculations we obtain a generalization of a Green medium [9, 10]:

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$$A_{ij} = \begin{bmatrix} A_{11} & & & \\ A_{11} - A_{66} & A_{11} & \text{sym} \\ A_{11} - A_{55} A_{11} - A_{44} & A_{11} & & \\ A_{41} & 0 & 0 & A_{44} \\ 0 & A_{52} & 0 & \frac{-A_{63}}{\sqrt{2}} & A_{55} \\ 0 & 0 & A_{63} & \frac{-A_{52}}{\sqrt{2}} & \frac{-A_{41}}{\sqrt{2}} & A_{66} \end{bmatrix}.$$
(23)

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Here

$$A_{41} = -2\sqrt{2}bc_2c_3; A_{44} = 2(a - bc_1^2);$$
  

$$A_{52} = -2\sqrt{2}bc_1c_3; A_{55} = 2(a - bc_2^2);$$
  

$$A_{53} = -2\sqrt{2}bc_1c_3; A_{56} = 2(a - bc_3^2),$$

while the operators T and D have the form

$$T = \{\partial_j, \epsilon_{jmn} c_m \partial_n, c_j \partial_{kk} - c_m \partial_{mj}\};$$
(24)

$$D_{1} = A_{11}\partial_{kk} - \rho\partial_{..},$$

$$D_{2} = \left[ (a - bc_{m}c_{m})\delta_{kl} + bc_{k}c_{l} \right]\partial_{kl} - \rho\partial_{..},$$

$$D_{3} = a\partial_{kk} - \rho\partial_{..},$$
(25)

where  $A_{11}$ , a, b,  $c_1$ ,  $c_2$ , and  $c_3$  are arbitrary parameters such that matrix (23) is positive definite [11, 12]. When b = 0, Eq. (23) yields an isotropic material.

If we replace  $\partial_k$  by  $n_k$  and replace  $\partial_{...}$  by  $|v|^2 = v_i v_i$  ( $v_i = |v| n_i$ ), we can use (25) to find the phase velocities corresponding to the wave normal  $n_k$ :

$$\rho |v|_{1}^{2} = A_{11}n_{k}n_{k} = A_{11},$$
  

$$\rho |v|_{2}^{2} = [(a - bc_{m}c_{m})\delta_{kl} + bc_{k}c_{l}]n_{k}n_{l} = a - bc_{m}c_{m} + bc_{k}c_{l}n_{k}n_{l},$$
  

$$\rho |v|_{2}^{2} = an_{k}n_{k} = a.$$

It is evident from (24) that Eqs. (23)-(25) define a medium with purely longitudinal and purely transverse waves [13], regardless of the direction of the wave normal  $n_k$ . Since  $|L| = |D| = D_1 D_2 D_3$ , it follows from (25) that the equations of the phase velocity surface and refraction surface [13] decompose into independent equations of three surfaces. These properties are essentially new properties for anisotropic materials, apart from the cases of isotropic and transversely isotropic materials [13, p. 165].

We now use (23) to find the strain energy:

$$2\Phi = A_{ij}\tilde{\epsilon}_{ij} = A_{11}(\epsilon_1 + \epsilon_2 + \epsilon_3)^2 + A_{44}(\epsilon_4^2 - 2\epsilon_3\epsilon_2) + A_{55}(\epsilon_5^2 - 2\epsilon_3\epsilon_1) + A_{66}(\epsilon_6^2 - 2\epsilon_2\epsilon_1) + A_{41}(2\epsilon_4\epsilon_1 - \sqrt{2\epsilon_6\epsilon_5}) + A_{52}(2\epsilon_5\epsilon_2 - \sqrt{2\epsilon_6\epsilon_4}) + A_{63}(2\epsilon_6\epsilon_3 - \sqrt{2\epsilon_5\epsilon_4})$$
(26)

 $(\varepsilon_1 = \varepsilon_{11}, \dots, \varepsilon_6 = \sqrt{2\varepsilon_{21}}$  represents strains). An expression that is similar to (26) but does not have the last three terms was presented in [10, p. 313] for 2 $\Phi$  for a Green medium. The author of [10] also wrote that Green's expression "is the most general form of the function  $\Phi$  for which the propagation of transverse plane waves is possible, i.e. for which the displacements will be parallel to the wave front." Equations (23) and (26) show that the expression in [10, p. 313] is not the most general form for  $2\Phi$ , since it has no terms with  $A_{41}$ ,  $A_{52}$ ,  $A_{63}$  – which may also be nontrivial.

If T has the form  $(\alpha_1 \neq \alpha_2 \neq \alpha_3 \neq 0)$ 

$$T = \begin{bmatrix} \alpha_1 \partial_1 & c_2 \alpha_3 \partial_3 - c_3 \alpha_2 \partial_2 & c_1 t_{p_1} t_{p_1} - c_n t_{n_1} \alpha_1 \partial_1 \\ \alpha_2 \partial_2 & c_3 \alpha_1 \partial_1 - c_1 \alpha_3 \partial_3 & c_2 t_{p_1} t_{p_1} - c_n t_{n_1} \alpha_2 \partial_2 \\ \alpha_3 \partial_3 & c_1 \alpha_2 \partial_2 - c_2 \alpha_1 \partial_1 & c_3 t_{p_1} t_{p_1} - c_n t_{n_1} \alpha_3 \partial_3 \end{bmatrix},$$
  
$$t_{p_1} t_{p_1} = \alpha_1^2 \partial_{11} + \alpha_2^2 \partial_{22} + \alpha_3^2 \partial_{33},$$
  
$$c_n t_{n_1} = c_1 \alpha_1 \partial_1 + c_2 \alpha_2 \partial_2 + c_3 \alpha_3 \partial_3,$$

then the Hooke's law matrix

$$A_{ij} = \begin{bmatrix} a + b\alpha_1^2 & & & \\ b\alpha_1\alpha_2 - a & a + b\alpha_2^2 & & \text{sym} \\ b\alpha_1\alpha_3 - a & b\alpha_2\alpha_3 - a & a + b\alpha_3^2 & & \\ 0 & 0 & 0 & 2a & \\ 0 & 0 & 0 & 0 & 2a \\ 0 & 0 & 0 & 0 & 2a \\ 0 & 0 & 0 & 0 & 0 & 2a \end{bmatrix},$$
(27)

Here, the characteristic operators

$$D_{1} = (a + b\alpha_{1}^{2})\partial_{11} + (a + b\alpha_{2}^{2})\partial_{22} + (a + b\alpha_{3}^{2})\partial_{33} - \rho\partial ,$$
  

$$D_{2} = D_{3} = a\partial_{\mu\nu} - \rho\partial .$$
(28)

In this equation, a, b,  $\alpha_i$ , and  $c_i$  are arbitrary parameters. The conditions of positive-definiteness of matrix (27) are as follows: a > 0, b > 0,  $b(\alpha_1\alpha_2 + \alpha_1\alpha_3 + \alpha_2\alpha_3) > \alpha$ . Material (27) is a special case of an orthotropic material. Let

$$T = \begin{bmatrix} \partial_1 & -\partial_2 & -\alpha \partial_{13} \\ \partial_2 & \partial_1 & -\alpha \partial_{23} \\ \alpha \partial_3 & 0 & \partial_{11} + \partial_{22} \end{bmatrix}, \quad \begin{array}{l} \alpha_1 = \alpha_2 = 1, \ \alpha_3 = \alpha, \\ c_1 = c_2 = 0, \ c_3 = 1, \end{array}$$

then [3]  $(\alpha^2 \neq 1)$ 

$$A_{ij} = \begin{vmatrix} A_{11} & & & \\ A_{21} & A_{11} & \text{sym} & & \\ A_{1i}\alpha - A_{33} & A_{31} & A_{33} & \\ \frac{A_{1i}\alpha - A_{33}}{1 - \alpha} & A_{31} & A_{33} & \\ 0 & 0 & 0 & \frac{2(A_{33} - A_{1i}\alpha^2)}{1 - \alpha^2} & \\ 0 & 0 & 0 & 0 & A_{44} & \\ 0 & 0 & 0 & 0 & 0 & A_{11} - A_{21} \end{vmatrix};$$
(29)

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$$D_{1} = A_{11}(\partial_{11} + \partial_{22}) + A_{33}\partial_{33} - \rho \partial ,$$
  

$$D_{2} = \frac{1}{2} (A_{11} - A_{21}) (\partial_{11} + \partial_{22}) + \frac{1}{2} A_{44}\partial_{33} - \rho \partial ,$$
  

$$D_{3} = \frac{1}{2} A_{44}\partial_{kk} - \rho \partial ...$$
(30)

Equations (29) define the subclass of transversely isotropic media. There are actual materials that conform to our relations; for example, for hexagonal crystals of cadmium [13], the parameter  $\alpha \approx 0.575$ .

If for example:

$$T = \begin{bmatrix} \partial_1 & -\partial_2 & \partial_{13} \\ \partial_2 & \partial_1 & \partial_{23} \\ -\partial_3 & 0 & \partial_{11} + \partial_{22} \end{bmatrix},$$

$$A_{ij} = \begin{bmatrix} A_{11} & & & \\ A_{21} & A_{11} & & \text{sym} & \\ -A_{11} & -A_{11} & A_{11} & & \\ 0 & 0 & 0 & A_{44} & \\ 0 & 0 & 0 & 0 & A_{44} & \\ 0 & 0 & 0 & 0 & A_{44} & \\ 0 & 0 & 0 & 0 & A_{11} - A_{21} \end{bmatrix};$$

$$D_{1} = A_{11}\partial_{kk} - \rho\partial ,$$

$$D_{2} = \frac{1}{2} (A_{11} - A_{21})(\partial_{11} + \partial_{22}) + \frac{1}{2} A_{44}\partial_{33} - \rho\partial ,$$

$$D_{3} = \frac{1}{2} A_{44}\partial_{kk} - \rho\partial .$$
(31)

Matrix (31) cannot be made positive definite. It is therefore physically impossible for a material with such elastic moduli to exist, even though all of the remaining conditions and equations are satisfied.

The examples presented above do not exhaust all of the cases in which Eqs. (1) reduce to three independent wave equations  $D\varphi = f$ . The other variants cannot be written out. As was noted above, Eqs. (28) and (30) can be used to find the phase velocities corresponding to the wave normal  $n_k$ , while the equations of the wave surfaces [13] decompose into independent equations of three surfaces.

Note. When we assign  $\alpha_{js}$  and find  $\beta_{jp}$  from the relation

$$\alpha_{js} \beta_{jp} = c_{sp} = \begin{bmatrix} 0 & -c_3 & c_2 \\ c_3 & 0 & -c_1 \\ -c_2 & c_1 & 0 \end{bmatrix},$$

we must consider all possible values of the parameters  $c_1$ ,  $c_2$ ,  $c_3$ , rather than just the variant in which all  $c_i$  are equal to zero. More general classes of anisotropic materials allowing the operators T and D can be obtained in certain cases for trivial values of  $c_i$ .

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## REFERENCES

- 1. N. I. Ostrosablin, "Toward the general solution of the equations of the linear theory of elasticity," Din. Sploshnoi Sredy (Sb. Nauch. Tr., AN SSSR, Sib. Otd-nie, In-t Gidrodinamiki), **92** (1989).
- 2. N. I. Ostrosablin and S. I. Senashov, "General solutions and symmetry of the equations of the linear theory of elasticity," Dokl. Akad. Nauk SSSR, 322, No. 3 (1992).
- 3. N. I. Ostrosablin, "General solutions and reduction of the system of equations of the linear theory of elasticity to diagonal form," Prikl. Mekh. Tekh. Fiz., No. 5 (1993).
- 4. V. Novatsky, Theory of Elasticity [Russian translation], Mir, Moscow (1975).
- 5. A. N. Norris, "On the acoustic determination of the elastic moduli of anisotropic solids and acoustic conditions for the existence of symmetry planes," Q. J. Mech. Appl. Math., 42, No. 3 (1989).
- 6. N. I. Ostrosablin, "Coefficient matrix in the equations of the linear theory of elasticity," Dokl. Akad. Nauk SSSR, **321**, No. 1 (1991).
- 7. N. I. Ostrosablin, "Equations of the linear theory of elasticity," Prikl. Mekh. Tekh. Fiz., No. 3 (1992).
- 8. L. V. Ovsyannikov, Group Analysis of Differential Equations [in Russian], Nauka, Moscow (1978).
- 9. J. J. Marciniak, "The generalized scalar wave equation and linear differential invariants in linear elasticity," Int. J. Eng. Sci., 27, No. 6 (1989).
- 10. A. Love, Mathematical Theory of Elasticity [Russian translation], ONTI NKTP SSSR, Moscow-Leningrad (1935).
- 11. N. I. Ostrosablin, "Narrowest ranges of the elastic constants and reduction of strain energy to canonical form," Izv. Akad. Nauk SSSR Mekh. Tverd. Tela, No. 2 (1989).
- 12. N. I. Ostrosablin, "Narrowest ranges of variation of the practical elastic constants of anisotropic materials," Prikl. Mekh. Tekh. Fiz., No. 1 (1992).
- 13. F. I. Fedorov, Theory of Elastic Waves in Crystals [in Russian], Nauka, Moscow (1965).